

### REMARKS

Claims 2-5 are pending herein. Claim 1 has been cancelled hereby without prejudice or disclaimer in favor of new claim 4. Claims 2 and 3 have been amended hereby to correct matters of form. Claim 2 has also been amended to depend from new claim 4. New claim 5 has been added hereby, as supported by the original specification. No new matter has been added.

1. The objection to Figure 5 is noted, but deemed moot in view of the Submission of New Formal Drawings filed herewith, in which the legend --Prior Art--has been added to Fig. 5. Accordingly, Applicant respectfully requests that the objection to the drawings be reconsidered and withdrawn.

Although not objected to, Fig. 1 has also been corrected to show Fig. 1A and Fig. 1B as separate drawing figures in the Submission of New Formal Drawings.

2. The §112, second paragraph rejection of claims 1-3 is noted, but deemed moot in view of the cancellation of claim 1 and in view of rewritten claims 2 and 3. Accordingly, Applicant respectfully requests that the above rejection be reconsidered and withdrawn.

3. Claim 1 was rejected under §102(e) over Sugimoto et al. ("Sugimoto"). To the extent that this rejection might be applied against new claim 4, it is respectfully traversed.

Claim 4 recites a light transmittable ceramic envelope for a high intensity discharge lamp, comprising a barrel section defining a discharge space, the barrel section having integrally formed end portions, and the end portions having an inner diameter smaller than an inner diameter of the barrel section to form electrode insertion sections protruding outwardly from the barrel section. A boundary portion between the barrel section and an inner portion of the electrode insertion sections has a radius of curvature R in a range of 0.01 mm to 3.0 mm.

An annotated reproduction of Sugimoto's Fig. 3 is provided on the on the following page. Contrary to the PTO's assertion, Applicant respectfully submits that there is no disclosure in Sugimoto that a boundary portion between the barrel section and an inner portion of the electrode insertion section has any radius of curvature, much less a radius of curvature in a range of 0.01 mm to 3.0 mm, as recited in claim 4. That is, as clearly shown in Fig. 3 of Sugimoto, the boundary, or corner portions, between the inner portion of the electrode insertion section and the barrel section are not rounded.

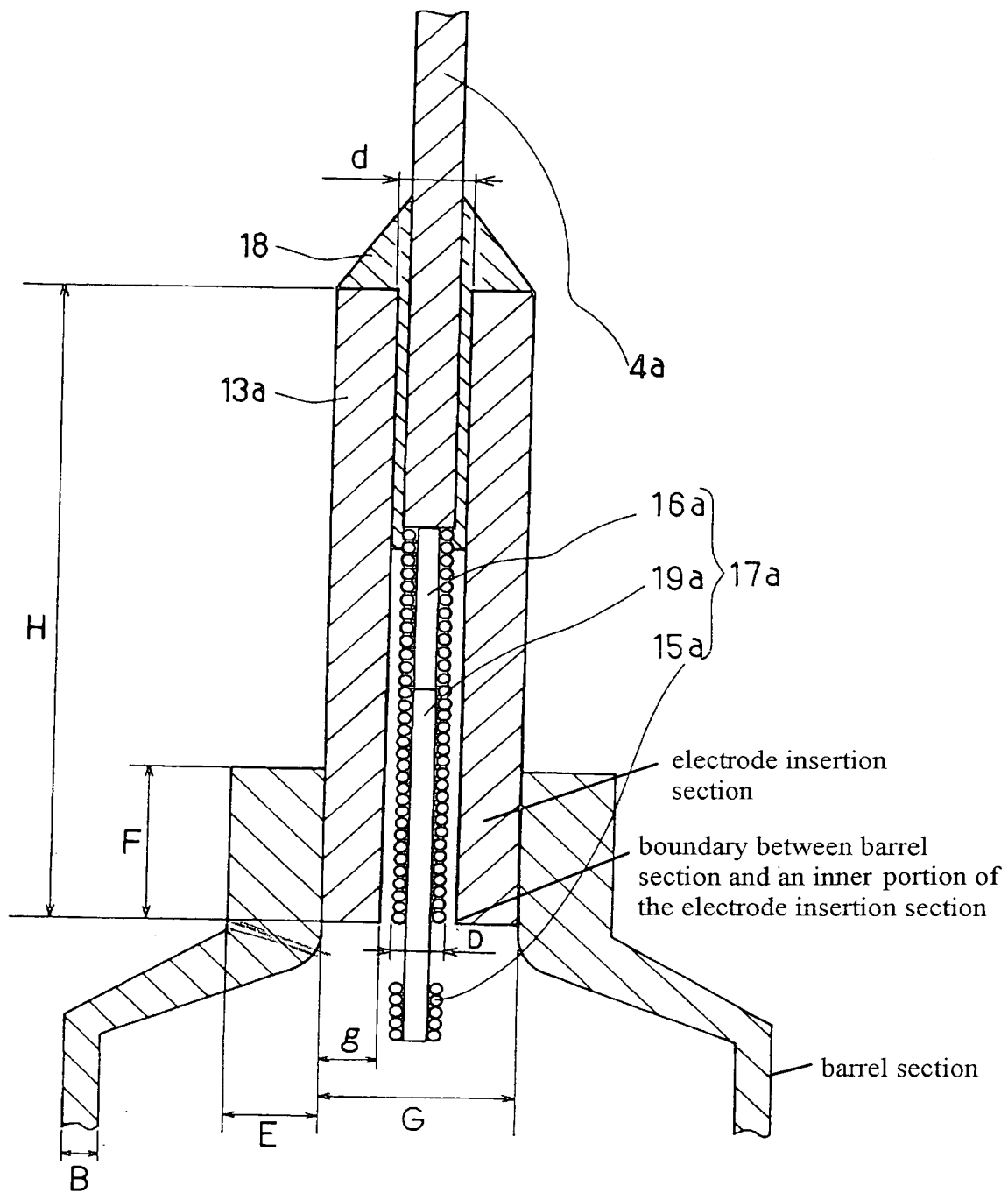


FIG. 3  
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Moreover, Applicant respectfully submits that Sugimoto does not disclose or suggest any reasons for providing a curved boundary portion between the barrel section and an inner portion of the electrode insertion section, much less the specific radius of curvature range recited in claim 4. Accordingly, Applicant respectfully submits that claim 4 is allowable over Sugimoto.

New dependent claim 5 submitted above further distinguishes the present application over Sugimoto. For example, new claim 5 recites that the barrel section is substantially elliptical. Applicant respectfully submits that Sugimoto does not disclose or suggest that the barrel section is substantially elliptical. Accordingly, Applicant respectfully submits that claim 5 should also be allowed.

For at least the foregoing reasons, Applicant respectfully submits that all claims pending herein define patentable subject matter over the art of record. Accordingly, Applicant respectfully requests that the above rejection be reconsidered and withdrawn.

4. Claims 2 and 3 were rejected under §103(a) over Sugimoto. Applicant respectfully traverses this ground of rejection.

Claim 2 depends from new claim 4, which is discussed above in section 3, and claim 3 depends from claim 2. Applicant respectfully submits that the arguments submitted above distinguish claim 4 from Sugimoto. Since claims 2 and 3 depend either directly or indirectly from claim 4, Applicant respectfully submits that these claims are also allowable over Sugimoto. Accordingly, Applicant respectfully requests that the above rejection be reconsidered and withdrawn.

5. **Applicant respectfully requests that the PTO acknowledge receipt and consideration of references AJ-AW cited in the Information Disclosure Statement filed on May 6, 2002.**

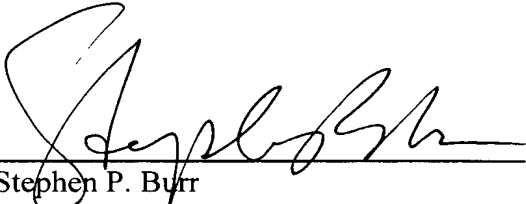
If the Examiner believes that contact with Applicant's attorney would be advantageous toward the disposition of this case, the Examiner is herein requested to call Applicant's attorney at the phone number noted below.

The Commissioner is hereby authorized to charge any additional fees associated with this communication or credit any overpayment to Deposit Account No. 50-1446.

Respectfully submitted,

May 22, 2003

\_\_\_\_\_  
Date

  
\_\_\_\_\_  
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Enclosures:

Appendix A - Substitute specification

Appendix B - marked-up specification

Submission of New Formal Drawings with 2 sheets of drawings (Figs. 1A, 1B and 5)

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## Specification

## Title of the Invention

## Ceramic Envelope for High Intensity Discharge Lamp

## Background of the Invention

## 1. Field of the Invention

The present invention relates to a ceramic envelope consisting of a light transmittable ceramic employed for a high intensity discharge lamp, such as a high intensity sodium lamp or a metal halide lamp, and particularly relates to a ceramic envelope for high intensity discharge lamp formed by integrally ~~molding~~forming electrode insertion section and at least end portions of a barrel section forming a discharge space.

## 2. Description of the Related Art

A discharge lamp employing a ceramic envelope made of light transmittable ceramics is advantageous in lamp efficiency, especially when the lamp has a discharge space formed into an ~~elliptic like~~elliptical shape by widening the diameter of a central section. Due to this, the discharge lamp is used in applications in which the lamp efficiency is regarded as particularly ~~regarded~~ important. The ~~A~~ ceramic envelope of this type has ~~a the~~ structure shown in FIG. 5, i.e., the ceramic envelope is formed such that an ~~elliptic like~~elliptical shape of barrel section 10 forming a discharge space is provided at ~~a the~~ center thereof. In addition, capillary tubes 11 serving as electrode insertion sections are integrally ~~molded~~formed with the both end portions of the barrel section 10 in a ~~long diameter~~longitudinal direction, while the capillary tubes 11 face each other. After light emission materials or starting gas is filled into the discharge space, ~~an electrode is~~electrodes are inserted into the capillary tubes 11, and then capillary tubes 11 ~~is~~are sealed to form a discharge lamp.

The ceramic envelope of such a shape is manufactured by ~~working to burning~~firing a ~~molded member~~ molded~~formed~~ by a ~~casting molding technique~~, a blowing technique, or a vacuum molding ~~technique~~techniques.

In case of the ceramic envelope having the integrally ~~molded~~formed barrel section 10 and the capillary tubes 11, each of the internal boundary end portions 12 between the barrel section 10 and the capillary tubes 11 ~~has~~have a relatively large radius R because of its manufacturing technique. Due to this, when the electrode is inserted and the lamp is assembled, a large space is formed between the electrode and the ceramic envelope. While the lamp is lighted up, the temperature of this space is relatively low since the space is distant from a ~~the~~ discharge section. As a result, the light emission materials in this space cannot be transformed into the materials in a gaseous phase but remain in the space in a liquid phase. This often causes an emission color change because the ratio of the light emission materials in the lamp changes thereby. In addition, these light emission materials, which are kept in the liquid phase, are exposed to high temperature while the lamp is lighted up. As a result, the ceramic envelope is gradually corroded and the extended service life of the lamp is impaired.

Moreover, since the linear transmittance of the ceramic envelope depends on surface roughness  $R_{max}$ , it is more advantageous to set the surface roughness  $R_{max}$  as small as possible. Nevertheless, while polishing can control the surface roughness of the inner surface of the ceramic envelope, the polishing step is complicated and not ~~rational~~practical. Further, if the envelope is polished, an additive such as MgO or  $La_2O_3$ , which ~~is~~are considered to be less resistant against halide than alumina, appears on the inner surface of the envelope. ~~That is to say that~~Thus, good discharge ~~characteristic~~characteristics cannot be maintained.

### Summary of the Invention

The present invention has been made in light of the above-stated problems. It is, therefore, an object of the present invention to provide a ceramic envelope for a high intensity discharge lamp formed by integrally ~~molding~~forming electrode insertion sections and at least end portions of a barrel section. This envelope is capable of reducing ~~the change of light color~~ changes of the high intensity lamp, and capable of extending the service life of the lamp.

According to a first aspect of the present invention, there is provided a ceramic envelope formed by integrally ~~molding~~forming at least end portions of a barrel section forming a discharge space and small-diameter electrode insertion sections, which are provided to protrude outward from the end portions of the barrel section, respectively; ~~the~~. The entire ceramic envelope is formed out of light transmittable ceramics. Further, a radius of curvature R is provided inside of a boundary end portion between the barrel section and at least one of said electrode insertion sections. A value of the R is set at in a range of 0.01 to 3.0 mm.

By specifying the value of the R provided on the corrodible boundary end portion between the barrel section and each electrode insertion section to be small, the quantity of remaining light emission materials in a liquid phase can be decreased. Thus, the service life of the lamp is extended and the change of light color is reduced. In this case, it is more preferable that the value of R is in a range of 0.1 to 1.0 mm. ~~The~~ A light emission tube having such value of R can be manufactured by ~~a~~-lost wax technique~~techniques~~, ~~a~~-powder press molding~~technique~~, ~~an~~-extrusion press molding~~technique~~, ~~a~~-frost molding~~technique~~, ~~an~~-injection molding~~technique~~ or ~~a~~-gel casting molding technique~~techniques~~.

According to a second aspect of the present invention, there is provided a ceramic envelope for high discharge lamp according to the first aspect of the invention, wherein a surface roughness  $R_{max}$  of an inner surface of the barrel section is set ~~at~~in a range of 0.01  $\mu\text{m}$  to 0.4  $\mu\text{m}$ , and ~~a~~the density of an additive on the inner surface of the barrel section is not more than half ~~a~~the density of the additive in a thick central portion of the barrel section.

By setting the  $R_{max}$  value as the above, ~~the~~a barrel section with a good light transmittable property can be provided, and the reaction of the light emission materials such as halide with the additive can be suppressed. As a result, good discharge e~~characteristic is~~characteristics are maintained. More preferably, the surface roughness  $R_{max}$  is in a range of 0.01  $\mu\text{m}$  to 0.1  $\mu\text{m}$ . It is noted that the density of the additive added to ~~ceramics~~the ceramic on the surface of the envelope is reduced by

the diffusion or splash action in the step of ~~burning~~firing the ~~molded~~formed member of the light emission tube. With this characteristic, the density of the additive on the surface can be set to be not more than half the density of the additive in the thick inside portion thereof. Due to this thin density of the additive, light emission materials such as halide can be suppressed from reacting with the additive and good discharge ~~characteristic~~characteristics can be maintained.

According to a third aspect of the present invention, there is provided a ceramic ~~envelopes~~envelope according to the second aspect of the invention, wherein the additive includes at least one material selected from a ~~the~~ group consisting of  $\text{Sc}_2\text{O}_3$ , ~~Mae~~MgO,  $\text{ZrO}_2$ ,  $\text{Y}_2\text{O}_3$  and a lanthanoid-based rare earth oxide.

By adding this additive, grains of the parent phase of ceramic represented by alumina are suppressed from abnormally growing, and thus uniform grain growth is induced. Moreover, the surface roughness  $R_{\text{max}}$  is controlled to have an appropriate value.

### **Brief Description of the Drawings**

FIGS. 1A and 1B are cross-sectional explanatory views showing one example of an embodiment of a ceramic envelope for a high intensity discharge lamp according to the present invention, where FIG. 1A is an overall view and FIG. 1B is a partially enlarged view;

FIG. 2 is a cross-sectional explanatory view showing another embodiment of the present invention;

FIG. 3 is a cross-sectional explanatory view showing yet another embodiment of the present invention;

FIG. 4 is a partially cross-sectional explanatory view showing yet another embodiment of the present invention; and

FIG. 5 is a cross-sectional explanatory view of a conventional ceramic lamp for a high intensity discharge lamp.



### Detailed Description of the Preferred Embodiments~~Invention~~

The embodiments of the present invention will be described hereinafter in detail with reference to the drawings.

FIG. 1 is a cross-sectional explanatory view showing one example of a ceramic envelope for a high intensity discharge lamp according to the present invention. The ceramic envelope includes a barrel section 1 which has a discharge space formed into an ~~elliptic-like~~elliptical shape with a diameter of central section widened. In addition, the ceramic envelope includes narrow-diameter capillary sections 2 serving as electrode insertion sections, which ~~is~~are formed by narrowing the right and left end portions of the barrel section 1. A rod-like current conductor (not shown) having a discharge electrode provided on a tip end is inserted and fixedly sealed into the capillary sections 2.

This ceramic envelope is ~~molded~~formed from materials mainly containing alumina by adding MgO as an additive, for example. After being ~~burned~~fired, the envelope has a light transmission property. The dimensions of the respective constituent elements will be shown by way of example. The outside diameter D1 of the barrel section 1 is 14.8 mm, the inside diameter D2 thereof is 13.0 mm, the length L1 thereof is 25.5 mm and the entire length L2 of light emission tubes is 55.7 mm. Also, the surface roughness Rmax of the inner surface of the envelope is set at 0.2  $\mu\text{m}$ . Each of the inside boundary end portions 3 between the barrel section 1 and the capillary sections 2 is formed to have ~~an~~a radius of curvature R of 1.0 mm as shown in a partially enlarged view of FIG. 1B.

The ceramic envelope having such an R value can be formed by ~~applying a lost wax technique, a powder press molding technique, an extrusion press molding technique, a frost molding technique, an injection molding technique or a gel casting molding technique~~techniques.

As stated above, by setting a relatively small R value in the corrodible boundary end portion between the barrel section and each electrode insertion section, ~~a~~the space in which light emission materials remaining in a liquid phase becomes

smaller. As a result, the occurrence of corrosion is ~~impaired~~ reduced and the service life of the lamp is extended. In addition, by decreasing the quantity of the light emission materials in the space, the unevenness of the change of light color can be reduced to 450 K (Kelvin) compared with the conventional unevenness of, for example, 600 K.

Further, grains of the parent phase of ceramic mainly consisting of alumina can be suppressed from abnormally growing, by adding the above-stated additive to alumina. Consequently, uniform grain growth is induced and linear transmittance is improved. It is noted that the surface roughness  $R_{max}$  is preferably in a range between 0.01  $\mu\text{m}$  and 0.4  $\mu\text{m}$  in a view of light transmittance and intensity. The additive may be  $\text{Sc}_2\text{O}_3$ ,  $\text{ZrO}_2$ ,  $\text{Y}_2\text{O}_3$ , or a lanthanoid-based rare earth oxide, or may be a combination thereof.

Further, in the step of ~~burning-firing~~ the molded ~~molded~~ formed member of the light emission tubes, the density of the additive added to alumina on the surface of the ~~molded~~ formed member is reduced by the diffusion or splash action thereof. With this characteristic, the density of the additive on the surface can be ~~set~~ controlled to be not more than half the density of the additive in the thick inside portion. By setting the density as ~~the~~ described above, the light emission materials such as halide are suppressed from reacting with the additive, and good discharge ~~characteristic~~ characteristics are maintained.

If the R value is less than 0.01 mm, ~~a~~ the crack occurrence frequency increases in a thermal shock ~~test~~ tests, and thus the end portions tend to be ~~end~~ damaged. On the other hand, if the R value exceeds 3.0 mm, the light emission materials tend to remain, as seen in a conventional light emission ~~tube~~ tubes, and thus the extended service life of the lamp cannot be obtained. For these reasons, it is preferable that the R value is ~~between~~ in a range of 0.01 and 3.0 mm, more preferably, between 0.1 and 1.0 mm.

For reference, in ~~the~~ thermal shock ~~test~~ tests, a light emission envelope heated in the air is put into the water. In this test, it is assumed that ~~(the~~ temperature of the light emission envelope before being put into the water at which temperature cracks

occur) —minus (the water temperature) = equals  $\Delta T$  ( $^{\circ}\text{C}$ ), and that thermal shock resistance becomes greater as  $\Delta T$  is higher. “n” represents the number of samples.

If  $R \geq 0.01$  and  $n = 10/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 190,

If  $R = 0$  and  $n = 10/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 170,

If  $R = 0.003$  and  $n = 10/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 180,

If  $R = 0.005$  and  $n = 3/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 180,

If  $R = 0.005$  and  $n = 7/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 190,

If  $R = 0.05$  and  $n = 10/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 190,

If  $R = 0.1$  and  $n = 3/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 190, and

If  $R = 0.1$  and  $n = 7/10$ ,  $\Delta T$  ( $^{\circ}\text{C}$ ) = 200.

This variation relates to the thermal shock resistance by repeating light-up / light-out and correlates with the service life of the lamp.

FIG. 2 is a cross-sectional explanatory view of a ceramic envelope showing another embodiment of the present invention. In this embodiment, the ceramic envelope is ~~molded~~formed by coupling two ~~molded~~formed members 5 and, 5 halved at a the center and having an ~~equal~~the same shape to ~~as~~ each other. Even if the ceramic envelope is formed as stated above, it is possible to ensure good additive density on the surface of the envelope and also possible to set the R value of each end portion to have an optimum value as in the case of the preceding embodiment. Besides, if the ceramic envelope consists of halves, the envelope can be easily ~~molded~~formed by injection molding or casting ~~molding~~.

FIG. 3 is a cross-sectional explanatory view of a ceramic envelope showing yet another embodiment of the present invention. In this embodiment, a the discharge space is formed as a cylindrical ~~like~~ shape. As shown in FIG. 3, a barrel section 6 forming a the light emission space is not necessarily ~~elliptic~~elliptical. Even with such a shape, ~~the~~ an extended service life of a lamp can be obtained by integrally ~~molding~~forming capillary sections 7 and the end portions of the barrel section 6, and further by providing a predetermined R value on the inside boundary end portion 8 between each capillary section 7 and the barrel section 6.

As shown in a partially cross-sectional explanatory view of FIG. 4, a shape of R that is provided inside of the boundary end portion between the barrel section and each electrode insertion section may be formed to protrude toward the center of the discharge space. Even with such a shape, the convection of light emission materials kept in a liquid phase can be reduced, and ~~the~~an extended service life of the lamp can be obtained as in the case of the preceding embodiments.

Furthermore, a region provided with the above-stated R may be one of the left and right corners of the discharge space. When a ceramic envelope is built vertically, light emission materials tend to remain in one of the corners which becomes a bottom. Due to this, only one of the corners which serves as the bottom may be provided to have the above-stated R value. In the above stated embodiments, an entire envelope is integrally ~~molded~~formed or an envelope is coupled with a left segment and a right segment. However, if an envelope, of which ~~an~~the inside diameter largely changes part of the ceramic envelope from the end portion of a barrel section to an electrode insertion section, is formed by integrally ~~molding~~forming, light emission materials in a discharge space can be reduced, and thus the service life of the lamp can be extended.

As stated so far in detail, the present invention can extend the service life of the lamp and reduce the change of light color. Additional advantages and modifications will readily occur to those skilled in the art. Therefore, the invention in its broader aspect is not limited to the specific details and representatives shown and described herein. Accordingly, various modifications may be made without departing from ~~The~~the spirit or scope of the general inventive concept as defined by the appended claims and their equivalents.